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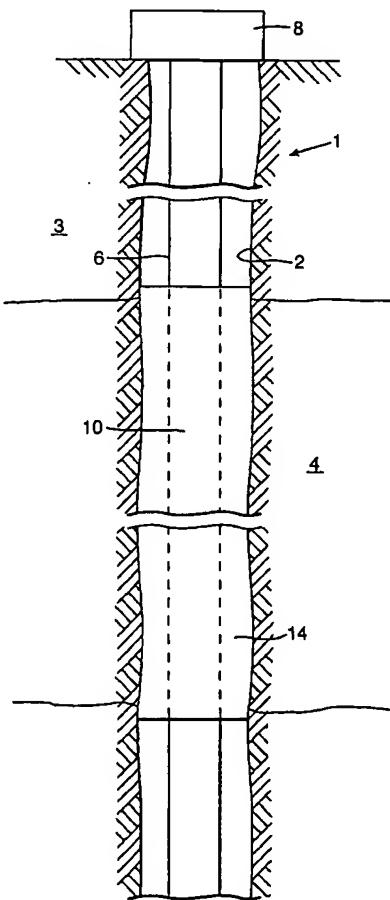
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*[Continued on next page]*

(54) Title: WELLBORE SYSTEM EXTENDING THROUGH A SALT LAYER



(57) Abstract: A wellbore system is provided including a wellbore formed in an earth formation, the wellbore extending into a salt layer of the earth formation. The wellbore system comprises a tubular conduit arranged in the wellbore whereby at least a portion of the tubular conduit is surrounded by the salt layer whereby an annular space is formed between said portion of the tubular conduit and the wellbore wall. The wellbore system further comprises an annular body of a resilient material arranged in said annular space and extending substantially the length of said portion of the tubular conduit surrounded by the salt layer.



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## WELLBORE SYSTEM EXTENDING THROUGH A SALT LAYER

The present invention relates to a wellbore system including a wellbore formed in an earth formation, the wellbore passing through a salt layer of the earth formation and being provided with a tubular conduit having a portion extending through the salt layer. Salt in a salt formation behaves as a plastic and exhibits creep when subject to differential stresses. If a wellbore is drilled through the salt formation, the in-situ stresses in the region around the wellbore alter.

For example, the horizontal in-situ stresses at the location of the wellbore before the wellbore is drilled, are replaced by horizontal stresses of magnitude corresponding to the hydraulic fluid pressure in the wellbore. If this fluid pressure is lower than the far field horizontal in-situ stresses in the salt formation, the salt in the vicinity of the wellbore will creep radially inward thus reducing the cross-sectional size of the borehole. Many times such radial deformation of the wellbore wall will be non-uniform, either in axial direction or in circumferential direction of the borehole. In view thereof, radial deformation of the wellbore wall can be more pronounced at some locations than at other locations so that a casing present in the wellbore can be subjected to locally high radial loading conditions as a result of the salt deformation. Non-uniform loading conditions can also occur if the borehole has an irregular shape due to, for example, washouts during drilling. Such irregularly shaped borehole will initially contact the casing at discrete points thereof

due to creep of the salt formation and will thereby potentially cause local damage to the casing, for example by buckling of the casing. If the casing has been cemented in the borehole, the cement would normally fill 5 the irregularities in the borehole and thus compensate for the non-uniform loading condition. However in many instances the cement not will not completely fill the borehole irregularities, especially if large washouts occur in the borehole.

10 Thus, there is a need for an improved wellbore system whereby a wellbore passes through a salt layer, which system reduces the risk of damage to the wellbore tubulars and overcomes the drawbacks of the prior art.

In accordance with the invention there is provided a 15 wellbore system including a wellbore formed in an earth formation, the wellbore extending into a salt layer of the earth formation, the wellbore system comprising a tubular conduit arranged in the wellbore whereby at least a portion of the tubular conduit is surrounded by the 20 salt layer, wherein an annular space is formed between said portion of the tubular conduit and the wellbore wall, the wellbore system further comprising an annular body of a resilient material arranged in said annular space and extending substantially the length of said 25 portion of the tubular conduit surrounded by the salt layer.

It is thereby achieved that the resilient material distributes the high radial loads caused by non-uniform 30 creep of the salt more uniformly along the length of the tubular conduit. Local overstressing of the tubular conduit due to such non-uniform creep is thereby prevented.

Suitably the annular body forms an annular layer provided to the outer surface of the tubular conduit, the annular layer extending continuously along substantially the length of said portion of the tubular conduit surrounded by the salt layer.

5 Instead of providing a continuous layer of resilient material in the annular space, a plurality of particles of resilient material can be inserted in the annular space to form a semi-continuous resilient annular body.

10 It is preferred that said resilient material is a swelleable material susceptible of swelling upon contact with a selected fluid. By swelling of the resilient material in the annular space, it is achieved that the resilient material fills up the annular space so that 15 axial flow of wellbore fluid through the annular space is thereby prevented. Moreover the swollen resilient material contacts the wellbore wall before significant creep of the salt formation occurs, and any tendency of the wellbore wall to deform non-uniformly is 20 substantially offset by counter-pressure from the swollen resilient material.

Suitably the swelleable material is an elastomer material, and the selected fluid is hydrocarbon fluid.

For example, the swelleable material includes at 25 least one of the group of natural rubber, nitrile rubber, hydrogenated nitrile rubber, acrylate butadiene rubber, poly acrylate rubber, butyl rubber, brominated butyl rubber, chlorinated butyl rubber, chlorinated polyethylene, neoprene rubber, styrene butadiene copolymer rubber, sulphonated polyethylene, ethylene acrylate rubber, epichlorohydrin ethylene oxide copolymer, ethylene-propylene-copolymer (peroxide crosslinked), ethylene-propylene-copolymer (sulphur

crosslinked), ethylene-propylene-diene terpolymer rubber, ethylene vinyl acetate copolymer, fluoro rubbers, fluoro silicone rubber, and silicone rubbers.

Preferred swelleable materials are EP(D)M rubber  
5 (ethylene-propylene-copolymer, either peroxide or sulphur crosslinked), EPT rubber (ethylene-propylene-diene terpolymer rubber), butyl rubber, brominated butyl rubber, chlorinated butyl rubber, and chlorinated polyethylene.

10 Suitably the hydrocarbon fluid is present in a stream of oil based drilling fluid pumped into the wellbore during drilling of the wellbore.

The present invention also relates to a method of creating a wellbore in an earth formation whereby the wellbore passes through a salt layer of the earth formation, the method comprising drilling said wellbore using a drilling fluid, arranging a tubular conduit in the wellbore wherein at least a portion of the tubular conduit is surrounded by the salt layer, and wherein an annular space is formed between said portion of the tubular conduit and the wellbore wall, the method further comprising arranging an annular body of a resilient material in the annular space so that the annular body extends substantially the length of said portion of the tubular conduit surrounded by the salt layer, said 20 resilient material being susceptible of swelling upon contact with the drilling fluid.  
25

Suitably the resilient material is an elastomer susceptible of swelling upon contact with oil based drilling fluid, and wherein the wellbore is drilled using said oil based drilling fluid.

30 Alternatively the wellbore is drilled using a water based drilling fluid, and the resilient material is an

elastomer susceptible of swelling upon contact with oil based fluid, and wherein said oil based fluid is pumped into the annular space so as to replace water based drilling fluid present in the annular space.

5        Optionally said oil based fluid is pumped into the wellbore as a stream in conjunction with a stream of cement for cementing the casing in the wellbore, the stream of oil based fluid and the stream of cement being spaced from each other.

10      The invention will be explained hereinafter in more detail by way of example, with reference to the accompanying drawings in which:

15      Fig. 1 schematically shows an embodiment of the wellbore system according to the invention, before swelling of the swellable material in the wellbore; and

Fig. 2 schematically shows an embodiment of the wellbore system according to the invention, after swelling of the swellable material in the wellbore.

20      Referring to Fig. 1 there is shown a wellbore system 1 including a wellbore 2 formed in an earth formation 3 having a salt layer 4 through which the wellbore 2 passes. A tubular conduit in the form of wellbore casing 6 extends from a wellhead 8 at surface, into the wellbore 2 whereby a portion 10 of the casing 6 extends through the salt layer 4. An annular space 12 is formed between the casing 6 and the wellbore wall. The portion 10 of casing 6 is provided with an annular layer 14 of EPDM rubber which is known to swell when in contact with hydrocarbon fluid, for example oil present in conventional oil based drilling fluid. The annular layer 14 has an initial thickness significantly smaller than the clearance between the casing 6 and the wellbore wall so as to allow unhampered lowering of the casing 6

with the annular layer 14 provided thereto, into the wellbore 2.

Referring further to Fig. 2, there is shown the wellbore system 1 after swelling of the annular layer 14 of EPDM rubber due to contact of the layer 14 with oil based drilling fluid present in the wellbore. The swollen annular layer 14 extends radially against the wellbore wall formed by the salt formation surrounding the wellbore 2. Thus, the annular space 12 vanishes after 10 swelling of the annular layer 14.

During normal operation the wellbore 2 is drilled in conventional manner using oil based drilling fluid. After drilling is completed, the casing 6 with the annular layer 14 provided thereto is lowered into the wellbore 2 and suspended in a position whereby the annular layer 14 extends substantially the length of the portion of the casing 6 passing through the salt layer 4. The annular layer of EPDM rubber thereby comes into contact with the oil based drilling fluid and starts swelling. Swelling of 15 the layer 14 continues for a period of time which can last several days, until the annular layer 14 completely occupies the annular space 12 and thus becomes biased against the wellbore wall at moderate pressure.

The salt in salt formation 4 near the wellbore wall tends to creep radially inward so that the diameter of 25 the wellbore portion passing through the salt layer 4 reduces slowly. As a result of the salt moving against the swollen annular layer 14, a compressive pressure builds up in the annular layer 14 of EPDM rubber. In many instances the salt will not uniformly creep radially inward along the length of the wellbore section passing 30 through the salt layer 4. Thus, there can be locations where the wellbore diameter reduces more than at other

locations due to the creeping salt, which would lead to locally severe loading conditions for the casing 6 if the rubber layer 14 would not be present between the casing 6 and the wellbore wall. Such severe loading is averted by  
5 the rubber annular layer 14 which deforms elastically due to the local load and thereby distributes the loading over a much larger area of the casing. The distributed load is of significantly lower magnitude than the high local loads to which the casing would be subjected in the  
10 absence of the annular layer 14, thus approaching uniform loading of the casing. In this manner it is achieved that failure of the casing due to locally severe loading conditions caused by non-uniform creeping of the salt, is prevented. Moreover, as a result of the more uniformly  
15 distributed compressive pressure between the salt at the wellbore wall and the swollen rubber layer, non-uniform creep of the salt along the length of the wellbore portion passing through the salt layer 4 is counter-acted.

20 From the above it will be understood that the swellable elastomer generates a pressure against the formation which delays the inflow of formation into the wellbore, and serves to spread concentrated loads acting on the casing from irregularities of the hole surface.  
25 The swelling pressure decreases with increasing amount of swelling and vice versa, i.e. there is an equilibrium between external pressures and internal pressures associated with the swelling mechanism. Thus, if after initial swelling of the elastomer the salt formation  
30 creeps radially inward and contacts the elastomer, the elastomer becomes locally compressed and exerts a back-pressure to maintain equilibrium. The swelling elastomer therefore not only spreads out concentrated loads from

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the creeping salt formation, but also pushes the salt formation back at a progressively increasing elastic force.

In a suitable alternative application the annular body of resilient material includes an annular body of sand.

C L A I M S

1. A wellbore system including a wellbore formed in an earth formation, the wellbore extending into a salt layer of the earth formation, the wellbore system comprising a tubular conduit arranged in the wellbore whereby at least 5 a portion of the tubular conduit is surrounded by the salt layer, wherein an annular space is formed between said portion of the tubular conduit and the wellbore wall, the wellbore system further comprising an annular body of a resilient material arranged in said annular space and extending substantially the length of said portion of the tubular conduit surrounded by the salt 10 layer.
2. The wellbore system of claim 1, wherein said annular body is provided as an annular layer to the outer surface 15 of the tubular conduit, said layer extending continuously along substantially the length of said portion of the tubular conduit surrounded by the salt layer.
3. The wellbore system of claim 1, wherein the annular body is formed from a plurality of particles of resilient 20 material inserted in said annular space.
4. The wellbore system of any one of claims 1-3, wherein said resilient material is a swelleable material susceptible of swelling upon contact with a selected fluid.
- 25 5. The wellbore system of claim 4, wherein the swelleable material is an elastomer material, and wherein the selected fluid is a hydrocarbon fluid.
6. The wellbore system of claim 5, wherein the swelleable material includes at least one of the group of

natural rubber, nitrile rubber, hydrogenated nitrile  
rubber, acrylate butadiene rubber, poly acrylate rubber,  
butyl rubber, brominated butyl rubber, chlorinated butyl  
rubber, chlorinated polyethylene, neoprene rubber,  
5 styrene butadiene copolymer rubber, sulphonated  
polyethylene, ethylene acrylate rubber, epichlorohydrin  
ethylene oxide copolymer, ethylene-propylene-copolymer  
(peroxide crosslinked), ethylene-propylene-copolymer  
(sulphur crosslinked), ethylene-propylene-diene  
10 terpolymer rubber, ethylene vinyl acetate copolymer,  
fluoro rubbers, fluoro silicone rubber, and silicone  
rubbers.

7. The wellbore system of claim 6, wherein the swellable  
material is selected from EP(D)M rubber (ethylene-  
15 propylene-copolymer, either peroxide or sulphur  
crosslinked), EPT rubber (ethylene-propylene-diene  
terpolymer rubber), butyl rubber, brominated butyl  
rubber, chlorinated butyl rubber, and chlorinated  
polyethylene.

20 8. The wellbore system of claim 6 or 7, wherein the  
hydrocarbon fluid is present in a stream of oil based  
drilling fluid pumped into the wellbore during drilling  
of the wellbore.

9. A method of creating a wellbore in an earth formation  
25 including a salt layer, the method comprising drilling  
said wellbore so that the wellbore extends into the salt  
layer, arranging a tubular conduit in the wellbore  
wherein at least a portion of the tubular conduit is  
surrounded by the salt layer, and wherein an annular  
30 space is formed between said portion of the tubular  
conduit and the wellbore wall, the method further  
comprising arranging an annular body of a resilient  
material in the annular space so that the annular body

extends substantially the length of said portion of the tubular conduit surrounded by the salt layer, said resilient material being susceptible of swelling upon contact with a selected fluid, and contacting said

5 resilient material with the selected fluid.

10. The method of claim 9, wherein the resilient material is an elastomer susceptible of swelling upon contact with oil based drilling fluid, and wherein the wellbore is drilled using said oil based drilling fluid.

11. The method of claim 9, wherein the resilient material is an elastomer susceptible of swelling upon contact with oil based fluid, wherein the wellbore is drilled using a water based drilling fluid, and wherein said oil based fluid is pumped into the annular space so as to replace

15 water based drilling fluid present in the annular space.

12.. The method of claim 11, wherein said oil based fluid is pumped into the wellbore as a stream in conjunction with a stream of cement for cementing the casing in the wellbore, the stream of oil based fluid and the stream of

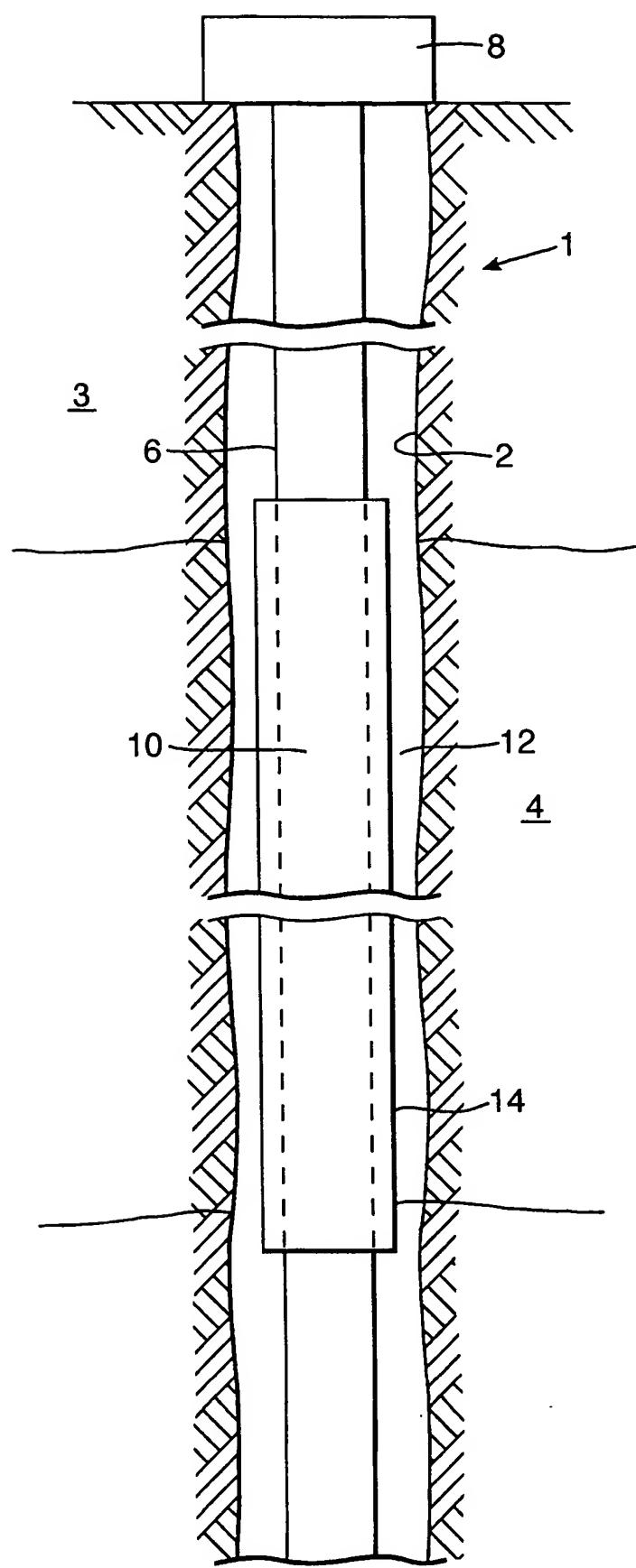
20 cement being spaced from each other.

13. The wellbore system substantially as described hereinbefore with reference to the accompanying drawings.

14. The method substantially as described hereinbefore with reference to the accompanying drawings.

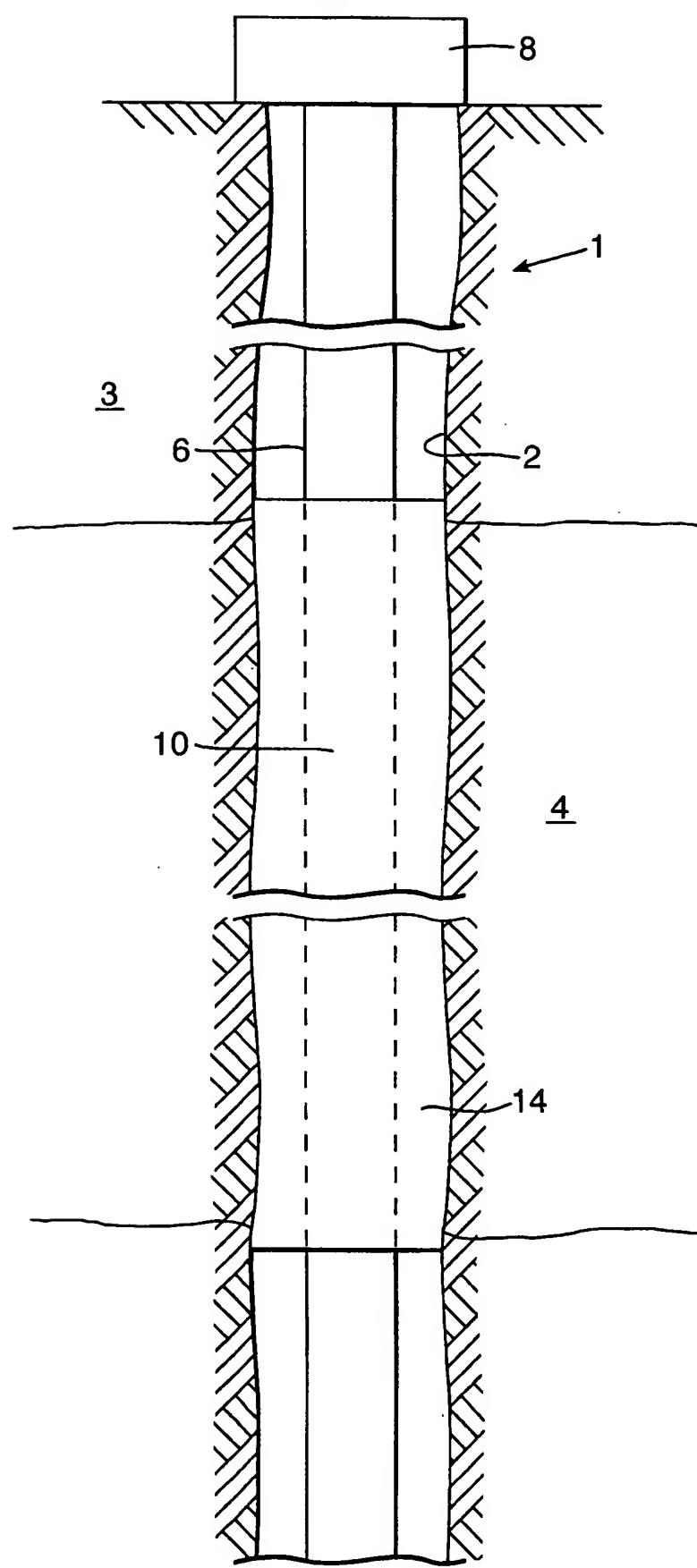
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Fig. 1.



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Fig.2.



## INTERNATIONAL SEARCH REPORT

International application No  
PCT/EP2005/056718

A. CLASSIFICATION OF SUBJECT MATTER  
E21B33/138 E21B33/127

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
E21B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the International search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, TULSA

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 2004/144538 A1 (RICHARD BENNETT M ET AL) 29 July 2004 (2004-07-29) the whole document	1-8,13, 14 9-12
X	US 4 462 714 A (SMITH ET AL) 31 July 1984 (1984-07-31) figure 2	1,2,13, 14
Y	PATTILLO, P. ET AL: "Effect of Nonuniform Loading on Conventional Collapse Resistance" SPE 79871, September 2004 (2004-09), XP002322970 the whole document	9-12
		-/-

Further documents are listed in the continuation of Box C.

See patent family annex.

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## INTERNATIONAL SEARCH REPORT

International application No  
PCT/EP2005/056718

### C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	WILSON, S. ET AL: "Assesment of Salt Loading on Well Casings" SPE 81820, 1 March 2003 (2003-03-01), XP002322971 the whole document -----	1
A	EP 1 300 545 A (SERVICES PETROLIERS SCHLUMBERGER; SCHLUMBERGER TECHNOLOGY B.V; SCHLUMB) 9 April 2003 (2003-04-09) paragraphs '0016!, '0018!, '0021!, '0025!; claim 18; figures 1-8 -----	1,8,13, 14
A	US 2004/055758 A1 (BREZINSKI MICHAEL M ET AL) 25 March 2004 (2004-03-25) figures 12-16,38-44 -----	1
A	WO 03/008756 A (SHELL INTERNATIONALE RESEARCH MAATSCHAPPIJ B.V; SHELL CANADA LIMITED;) 30 January 2003 (2003-01-30) -----	1,9,13, 14
A	WO 2004/057715 A (FREYER, RUNE) 8 July 2004 (2004-07-08) page 6, lines 3-9 -----	4-12

**INTERNATIONAL SEARCH REPORT**

Information on patent family members

International application No PCT/EP2005/056718	
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Patent document cited in search report	Publication date		Patent family member(s)	Publication date
US 2004144538	A1	29-07-2004	AU 2004208145 A1 CA 2514967 A1 GB 2414259 A WO 2004067906 A1	12-08-2004 12-08-2004 23-11-2005 12-08-2004
US 4462714	A	31-07-1984	NONE	
EP 1300545	A	09-04-2003	WO 03031768 A1 US 2004261998 A1	17-04-2003 30-12-2004
US 2004055758	A1	25-03-2004	AU 2003270795 A1 BR 0314637 A CN 1708631 A EP 1552105 A2 WO 2004027201 A2 US 2005023003 A1 US 2005092485 A1	08-04-2004 02-08-2005 14-12-2005 13-07-2005 01-04-2004 03-02-2005 05-05-2005
WO 03008756	A	30-01-2003	BR 0211253 A CA 2453660 A1 CN 1533465 A EA 5440 B1 US 2004261990 A1	27-07-2004 30-01-2003 29-09-2004 24-02-2005 30-12-2004
WO 2004057715	A	08-07-2004	AU 2003303119 A1 BR 0317127 A CA 2506923 A1 EP 1570151 A2 NO 318358 B1	14-07-2004 25-10-2005 08-07-2004 07-09-2005 07-03-2005